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Evaluating the Potential Groundwater Availability within a Lower Trinity Aquifer Well Field, Balcones Fault Zone, Hays County, Central Texas

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SUMMARY

Groundwater availability from the Edwards and Middle Trinity Aquifers in the study area is generally limited, however, the Lower Trinity Aquifer within the study area is untested because of the aquifer depths, assumed low yields, and poor water quality. This study provides an initial assessment of groundwater availability in a Lower Trinity well field based on aquifer tests, geochemistry, and limited analytical modeling.

The well field contains three wells spaced about 1/3 mile apart that range in total depths from 1,505 to 1,620 ft below ground surface. Depths to static water levels in the wells range from 140 to 150 ft below ground surface. Aquifer testing involved an initial single well test in 2018 followed by a test that pumped the two newer wells drilled in 2019 at 170 gallons per minute (gpm) independently for 96 hrs each, while monitoring the other wells. Maximum drawdown in the pumped wells ranged from 320 to 460 ft. Drawdown in the observation wells (0.2 to 0.4 miles distant) ranged from 8 to 34 ft. To estimate aquifer parameters, continuous water-level data were collected with transducers and fit to Theis and Cooper-Jacob analytical solutions using Aqtesolv software. Results of transmissivity from observation wells averaged about 401 ft²/day and a storativity of 5.57-E05. These parameters are higher than published median values of Lower Trinity wells in the Hill Country to the west of the study area.

Specific conductance of groundwater was monitored throughout the aquifer test and groundwater samples were analyzed for total dissolved solids (TDS) resulting in values of about 560 mg/L, indicating fresh water. Ion geochemistry indicates a calcium bicarbonate (Ca-HCO₃) water with a tritium value of -0.05 TU, and a carbon-14 value of 0.006 percent modern carbon, PMC, indicating very old water.

Using parameters from the aquifer test and analytical models we forecasted drawdown from the well field with a combined pumping rate of 380 gpm (200 MGY) over a 30-year period. Preliminary analytical model results indicate an estimated drawdown up to about 130 ft at a distance of 2.0 miles from the well field.

Because the results of the aquifer test indicate that the water quality and yield of these wells are high. the Lower Trinity Aquifer may be a direct alternative groundwater supply for the study area. More groundwater studies and modeling are needed to evaluate long-term drawdown effects for the study area. The nearby Lower Trinity Aquifer of western Travis County offers a cautionary example of groundwater mining. In addition, the aquifer may have potential for aquifer storage and recovery (ASR) activities.

This summary was modified from a presentation and published abstract at the 2020 Geological Society of America South-Central Meeting (Camp et al., 2020).

INTRODUCTION

Several potential groundwater resources occur within the jurisdiction of the Barton Springs/Edwards Aquifer Conservation District (BSEACD) and includes the Edwards and Trinity Aquifers. The Edwards Aquifer is well characterized but has very limited and conditional groundwater availability (Hunt et al., 2019). Recent studies have dramatically increased the information on the Middle Trinity Aquifer (Smith et al., 2018), but there is still uncertainty in the availability and an increasing demand on the Middle Trinity Aquifer. However, the Lower Trinity Aquifer has unknown groundwater availability potential as there are generally few wells completed within the Lower Trinity within BSEACD. The owner of the well field referred to as the "Gragg" tract (**Figure 1**) decided to test the groundwater availability potential of the Lower Trinity Aquifer. A single well was drilled (Gragg #1) and a pumping test was performed by Geos Consulting (2018) in early 2018. Results indicated fresh water (542 mg/L TDS) and relatively high well yields (115 gpm). Those results led to the completion of two additional test wells (Gragg #2 and #3) in September and October 2019.

Given the mutual interests of understanding the Lower Trinity Aquifer as a groundwater resource, BSEACD staff assisted in the additional aquifer testing of the Lower Trinity in 2019. An aquifer test was designed (**Appendix D**), and data collected, by BSEACD in cooperation with Bee Cave Drilling and the land owner Bill Walters. This report presents the aquifer test results of the Lower Trinity Aquifer in the Gragg wells 1, 2 and 3. The aquifer tests provide important information about the aquifer, well yields, and water quality and will be critical to inform any future production permit request for the Gragg well field (wells 1-3). The well owner indicated a potential future demand of up to 200,000,000 gallons per year (gpy) from the Gragg well field, which helped guide the design of the test.

Gragg Well Field

The Gragg well field is located on a 325-acre property of historically agricultural land along Old Bliss Spillar Road west of State Highway 45 (**Figure 1**). The well field consist of three Lower Trinity wells: Gragg #1 (SDR 473734; TWDB 58-50-755), Gragg #2 (SDR 527500) and Gragg #3 (SDR 527505) (**Appendix A**). Gragg #1 specific capacity testing was done in 2018. The Gragg #2 and Gragg #3 wells, the focus of this memo, were pumped in 2019 and utilized the adjacent wells as observation wells.



Figure 1. Site map of Gragg well field in Hays County located at Old Bliss Spillar Rd., Manchaca, TX. The wells are spaced ranging from 0.2 to 0.4 miles apart.

Hydrogeological setting

The Gragg tract and well field is located within the Balcones Fault Zone and bound by several mapped faults in the area. Bedrock consists of the Georgetown Fm and is overlain by a relatively thick soil (**Figure 2**). The well field area is underlain by the Edwards Aquifer and is considered part of the recharge zone of the Edwards Aquifer.

The target for the production and test wells is the Lower Trinity Aquifer, which is the deepest known aquifer in the area, occurring below the Edwards and Middle Trinity aquifers. The depth to the top of the Lower Trinity Aquifer is about 1,300 ft below surface at the wells (Figures 3 and 4). Stratigraphic picks were made from geophysical logs (Appendix B) collected at both Gragg #2 and #3 wells after their completion. Stratigraphic contacts are indicated on Table 1.

The Lower Trinity Aquifer is estimated to be about 450-500 ft thick in the area and is confined by the overlying Hammett Shale and other geologic units (Hunt et al, 2020). The Hammett is a ubiquitous shale that behaves as a regional aquitard between the overlying Middle Trinity and underlying Lower Trinity Aquifer units. The Lower Trinity Aquifer is composed of the Sligo and Hosston formations. The Hosston (Sycamore Sand equivalent) consists of terrigenous, clastic, fine- to coarse-grained feldspathic sandstone and cobble conglomerate and unconformably overlays the Paleozoic (Ouachita Facies) basement. The Hosston is exposed along the Pedernales and Colorado River valleys in western Travis County. The Sligo Formation is a shallow-water, high-energy carbonate that pinches out to the west prior to reaching the Pedernales River Valley.

Recharge to the Lower Trinity is generally thought to occur from leakage from overlying units through the Hammett Shale and along fractures and faults that breach the shale. Groundwater within the Lower Trinity Aquifer is thought to be within a deeply confined and compartmentalized aquifer system containing very old (1,000s of years) groundwater moving very slowly through a diffuse matrix.

The wells were drilled by Bee Caves Drilling Inc. using air rotary methods and were cemented from the top of the Sligo to the surface using the positive displacement method. Well construction is summarized in **Table 2** and driller's reports are in **Appendix A**. Well schematics for Gragg well #2 is shown in **Figure 4** and wells #1 and #3 are shown in **Appendix C**.

| Geologic Formation | Gragg #2 depth (ft) | Gragg Well #3 depth from surface (ft) | Average Thickness (ft) | Comment |
|---------------------------|------------------------|------------------------------------------|---------------------------|--------------------------------------------------------|
| Soil | surface | surface | | Soil |
| Georgetown (Kgt) fm | 7 | 7 | | partial thickness, eroded (normally 50 ft thick) |
| Edwards Group (Ked) | 20 | 20 | 445 | |
| Walnut (Kwal) fm | 412 | 435 | 41 | |
| Upper Glen Rose (Kgru) | 453 | 476 | 519 | |
| Lower Glen Rose (Kgrl) | 973 | 993 | 210 | |
| Hensel (Khe) fm | 1183 | 1202 | 27 | |
| Cow Creek (Kcc) fm | 1212 | 1226 | 82 | |
| Hammet (Kha) fm | 1291 | 1310 | 41 | |
| Sligo (Ksl) fm | 1332 | 1351 | 85 | |
| Hosston (Kho) fm | 1415 | 1437 | 274 | Minimum thickness; not fully penetrated |
| Total borehole depth | 1700 | 1700 | | |

Table 1. *Stratigraphic contacts of Gragg wells #2 and #3 determined by geophysical logs.*

 Table 2. Well information and construction summary. Detailed records within Appendix A.

| Parameter | Gragg #1 | Gragg #2 | Gragg #3 |
|---------------------------------|--------------------|----------------------------|----------------------------|
| Tracking number (SDR) | 473734 | 527500 | 527505 |
| State well number (TWDB) | 58-50-755 | | |
| Latitude | 30.134734° | 30.131514° | 30.130953° |
| Longitude | -97.866928° | -97.867811° | -97.861429° |
| Land surface elevation (ft-msl) | 742 | 732 | 722 |
| Date completed | 1/26/2018 | 9/25/2019 | 10/10/2019 |
| Total depth (ft) | 1620 | 1700 | 1700 |
| Depth of casing (ft) | 1434 | 1350 | 1355 |
| Diameter of casing (in) | 8* | 8.625 | 8.625 |
| Open hole or slotted interval | Slotted 180 ft | Open 350 ft (1350-1700 ft- | Open 345 ft (1355-1700 ft- |
| | (1434-1614 ft-bgs) | bgs) | bgs) |
| Diameter of open or slotted | 5.0 | 7.875 | 7.875 |
| interval | | | |
| Water level (ft-bgs) | 196 (1/8/2018) | 136 (10/18/2019) | 132 (10/18/2019) |
| Reported yield (gpm) | 115 | 170 | 170 |
| Aquifer test date | 2/1/2018 | October 18-22, 2019 | October 24-28, 2019 |
| Distance to Gragg #3 (ft) | 2,215 | 2,028 | 0 |

*telescoping casing (8 in 0-1342 ft, 5 in 1334-1434 ft)



Figure 2. Geologic map of the well field area (Hauwert, 2008). The well field is on the eastern edge of the Edwards Recharge Zone. Numerous faults are mapped in the area.



Figure 3. Geologic and hydrogeologic cross section through study area. Potentiometric surfaces are inferred based upon measured water levels in the wells. Values are shown as depth from surface. Modeled water level (dashed line) is based upon static levels and results from analytical models with parameters derived from the aquifer testing in this report.



Figure 4. Schematic of Gragg #2 well construction and stratigraphy with modeled water levels for 4-day and 30-yr pumping scenarios. Stratigraphic picks made from the geophysical log. Actual measured drawdown in well during Gragg #2 aquifer test was 573.0 ft-dtw.

AQUIFER TEST

In order to achieve the mutual interests of an aquifer test, BSEACD staff helped design the 2019 aquifer test of the Gragg tract well field. A work plan was developed (**Appendix D**) and designed to satisfy the District's guidelines (BSEACD, 2016) for an aquifer test that could support a potential permit request of up to 200 MGY for this well field (Gragg Wells #1-3) in the future. The goal of the test was to produce three times the potential daily volume of about 1.6 million gallons per day, which was estimated to be 96 hrs of pumping at a rate of about 150 gpm for each well. Gragg #1 was not pumped as part of the 2019 aquifer testing but was used as an observation well during the testing and is therefore included as part of the well field.

An aquifer test was conducted for the Gragg #2 and #3 wells over two separate 4-day periods to allow for pumping and recovery. During Gragg #2 pumping, Gragg #1 and #3 were used as observation wells. During Gragg #3 pumping, Gragg #1 and #2 were used as observation wells. Gragg #1 was solely used as an observation well in the 2019 testing. However, information on the Gragg #1 yield, water quality, and drawdown was evaluated from a single-well testing in 2018 (Geos Consulting, 2018). Locations of the pumped and monitored wells are shown in **Figure. 1**. A summary of the aquifer testing information are provided in **Tables 3-5** and hydrographs provided in **Figures 6-8**.

Prior to the start of each 4-day testing period, BSEACD staff installed absolute (non-vented) pressure transducers on a stainless steel cable in each of the observation wells, and a gauged (vented) pressure transducer with vented cable in the pumping well. Water levels in the observation wells taken by the non-vented pressure transducers were confirmed by staff taking periodic manual measurements during the test using an electric measuring tape (E-line). Pumping rates were calculated by reading an inline flowmeter three times and taking the average.

Due to the deeply confined nature and distance from its recharge area, the Lower Trinity Aquifer is less susceptible to surface hydrologic processes during aquifer testing. As such, surface hydrologic conditions, such as rainfall, did not influence the results of any of the testing. Instead, an effort to monitor the static water level over a period of days prior to the testing was done to understand background trends.



Figure 5. Photographs of Gragg #2 Aquifer Test (taken on 10/18/2019).

Gragg #1 Test

A single well test was conducted in 2018 on Gragg #1. This was the initial test well of the Lower Trinity in the area. Information on the single-well testing was provided by Geos Consulting (2018) and summarized in **Table 3**.

Table 3. Aquifer test summary for Gragg #1 on February 2018. Gragg wells #2 and #3 were not yet drilled during the testing.

| | Gragg #1 | Comment |
|-----------------------------|----------------|---------|
| Pumping start | 2/1/2018 10:40 | |
| Pumping stop | 2/1/2018 16:10 | |
| Duration (hrs) | 5.5 | |
| Pumping rate (gpm) | 115 | Max 155 |
| Static water level (ft-bgs) | 138 | |
| Maximum drawdown (ft) | 431 | |
| Specific capacity (gpm/ft) | 0.27 | |
| Recovery (hrs to 90%) | 1 | |
| Total volume pumped (gal) | ~44,550 | |



Figure 6. Hydrograph of the Gragg #1 single-well pumping test from 2018 (data from Geos Consulting, 2018).

Gragg #2 Test

The Gragg #2 aquifer test data are summarized in **Table 4**. Static background water levels were collected in Gragg wells #1 and #3 with non-vented pressure transducers for 7 days prior to initiating the Gragg #2 aquifer test. Background water-level data show a discernable downward trend prior to the start of Gragg #2 aquifer test. Non-vented pressure transducers in observation wells #1 and #3 were set at 320 ft bgs and 400 ft bgs, respectively, and set to take measurements at 15-minute intervals. In well #2 a 915-ft tremie pipe was installed with the test pump to allow the vented pressure transducer to take measurements at 600 ft bgs at 1-minute intervals. All pressure transducers remained in place throughout the test and until the water level in the pumping well had reached 90% recovery.

Static water level in the Gragg #2 pumping well was 136 ft bgs. Static water levels in Gragg #1 and #3 were 133 ft bgs and 145 ft bgs, respectively. Maximum measured drawdown in the pumping well over 96 hours (5,760 minutes) was a total of 437 ft, and in observation wells #1 and #3 was 34 ft and 17 ft, respectively. The average pumping rate was 168 gpm. Upon turning the well pump off, the water level recovered 418 ft (143.5 bgs) within 1 hour (~90%, **Figure 7**). A total of 915,400 gallons were pumped from Gragg #2.

| 10000 10100000 $1000000 100000 100000 10000000000$ | Table 4. | Aquifer | Test Summ | ary for Gra | gg #2 on | October | 18-22, | 2019 |
|------------------------------------------------------|----------|---------|-----------|-------------|----------|---------|--------|------|
|------------------------------------------------------|----------|---------|-----------|-------------|----------|---------|--------|------|

| | Gragg #1 | Gragg #2 | Gragg #3 | Comment |
|-----------------------------|----------|------------------|----------|---------|
| Pumping start | N/A | 10/18/2019 10:00 | N/A | |
| Pumping stop | N/A | 10/22/2019 10:00 | N/A | |
| Duration (hrs) | N/A | 96 | N/A | |
| Pumping rate (gpm) | N/A | 168 | N/A | Max 178 |
| Static water level (ft-bgs) | 133 | 136 | 145 | |
| Maximum drawdown (ft) | 34 | 437 | 17 | |
| Specific capacity (gpm/ft) | N/A | 0.38 | N/A | |
| Recovery (hrs to 90%) | | 1 | | |
| Total volume pumped (gal) | N/A | 915,400 | N/A | |



Figure 7. *Hydrograph of Gragg #2 pumping well (blue) and Gragg #1 and #3 observation wells (green and purple, respectively) during pumping and recovery phases of the aquifer test. Note the vertical change in scale.*

Gragg #3 Test

The Gragg #3 aquifer test data are summarized in **Table 5**. Prior to pumping Gragg #3, static background water levels were collected in Gragg wells #1 and #2 during well #3 pump installation. Procedures and setup for the pumping and observation wells in the Gragg #2 aquifer test were applied to Gragg #3.

The static water level in the Gragg #3 pumping well was 141 ft bgs while the static levels in Gragg #1 and #2 were 151 ft bgs and 141 ft bgs, respectively. The maximum measured drawdown in the pumping well *Technical Memo 2020—0630* Page 12 of 70 over 93 hours (5,580 minutes) of pumping was 320 ft and in observation wells Gragg #1 and #2 was 8 ft and 9 ft, respectively. The average pumping rate was 175 gpm. Upon turning the well pump off, the water level recovered 320 ft to 141 ft bgs in 1 hour. (~90 %, **Figure 8**). A total of 901,300 gallons were pumped from Gragg #3. Observation wells were still recovering 52 hours after the Gragg #2 test (**Figure 8**) because it represents the combined (slow) recovery from Gragg #2 and #3 pumping.

| | Gragg #1 | Gragg #2 | Gragg #3 | Comment |
|-----------------------------|----------|----------|------------------|---------|
| Test start | N/A | N/A | 10/24/2019 16:00 | |
| Test stop | N/A | N/A | 10/28/2019 12:00 | |
| Duration (hrs) | | | 93 | |
| Pumping rate (gpm) | | | 175 | Max 200 |
| Static water level (ft-bgs) | 151 | 141 | 141 | |
| Maximum drawdown (ft) | 8 | 9 | 320 | |
| Specific capacity (gpm/ft) | N/A | N/A | 0.54 | |
| Recovery (hrs to 90%) | | | 1 | |
| Total volume pumped (gal) | N/A | N/A | 901,300 | |

 Table 5. Aquifer test summary for Gragg #3 on October 24-28, 2019



Figure 8. Hydrograph of Gragg #3 pumping well (blue) and Gragg #1 and #2 observation wells (green and purple, respectively) during pumping and recovery phases of the aquifer test. Note the vertical change in scale. After the test, the recovery of water levels in the observation wells are above the zero line because at the start of Gragg #3 test the water levels had not fully recovered from pumping of Gragg #2. Thus, the water-level recovery is combined from the Gragg #2 and #3 pumping.

PARAMETER ESTIMATION

Data from the pumping and recovery phases of each aquifer test were analyzed using Aqtesolv software to determine hydraulic properties of the Lower Trinity Aquifer (Figure 9). Aqtesolv (Duffield, 2007) is a commercial software package developed for the design and analysis of aquifer-test data. The software provides a model of the theoretical response to pumping for the given input parameters. Aqtesolv is an important tool used by the District to analyze aquifer-test data. The software provides a comprehensive suite of analytical solutions for confined aquifers such as Theis (1963) and Cooper-Jacob (1946).



Figure 9. Example of results from AqteSolv software analysis of Gragg #3 observation well during Gragg #2 pumping and recovery phases of the aquifer test. There is a very good match of the modeled (solid line) and observed (symbols) data.

Aqtesolv allows for assigning multiple wells to an X and Y coordinate system, pumping duration, and well construction information (**Table 2**). Detailed pumping times and rates were directly imported into the software. Aquifer-test data were formatted into elapsed time (minutes) and drawdown (ft). The thickness of the aquifer was determined to be about 350 ft from geophysical logs (**Table 1**). The ratio of vertical to horizontal permeability (Kv/Kh) was estimated to be about 0.1. Note that the resulting estimates of the aquifer parameters are generally insensitive to changes in these (thickness, Kv/Kh) parameters.

Analyses of the data included considerations such as: 1) late-time data for a given test are generally more representative; 2) distant observation wells generally provide a better estimate of storativity; 3) drawdown data from pumping wells generally show high levels of head loss; and 4) deviations of the observation data from theoretical (model) type curves can illuminate processes within the aquifer such as boundary conditions. Identification of boundary conditions is critical to the evaluation of the aquifer test (Duffield and Butler, 2015).

The Theis solution fits the observation data better than most other analytical solutions such as straight-line or recovery methods. The use of those straight-line and recovery solutions generally results in elevated aquifer parameters when compared to Theis (**Table 5**). In addition, we determined that the Theis solution fits the data better than other solutions that consider leaky or fractured aquifers. No boundary conditions were observed under the conditions of the test.

Results of transmissivity (T) from pumping and observation wells are summarized in **Table 5**. A summary of the average of the best-fit values using Theis solution is provided in **Table 6**. The average values include a transmissivity value of 401 $\text{ft}^{2/}$ day and a storativity of 5.57-E05. These parameters are higher than published median values of Lower Trinity wells in the Hill Country to the west of the study area (Hunt et al., 2010; Hunt et al., 2020).

| Well Name | Т | Т | S | Analytical Solution |
|----------------------|-----------|-----------|-----------|---------------------|
| | (ft2/day) | (gpd/ft2) | | |
| Gragg #2 Pumping Wel | 1 | | | |
| Gragg # 2 Pumping | 104.0 | 778.0 | 5.34E-05 | Cooper-jacob |
| Gragg # 2 Pumping | 100.5 | 751.8 | 9.11E-05 | Theis |
| Gragg #1 Obs | 266.2 | 1991.3 | 3.73E-05 | Theis |
| Gragg #1 Obs | 262.6 | 1964.4 | 3.84E-05 | Cooper-Jacob |
| Gragg #3 Obs | 402.3* | 3009.4* | 5.97E-05* | Theis |
| Gragg #3 Obs | 403.0* | 3014.6* | 4.83E-05* | Cooper-Jacob |
| Gragg #1, 3 Obs | 402.1 | 3007.9 | 6.07E-05 | Theis |
| Gragg #1, 3 Obs | 431.7 | 3229.3 | 4.27E-05 | Cooper-Jacob |
| Gragg # 1, 2, 3 | 402.1 | 3007.9 | 6.18E-05 | Theis |
| Gragg # 1, 2, 3 | 317.0 | 2371.3 | 2.34E-05 | Cooper-Jacob |
| Gragg #1, 2 | 262.6 | 1964.4 | 3.84E-05 | Theis |
| Gragg #1, 2 | 319.7 | 2391.5 | 2.35E-05 | Cooper-Jacob |
| Gragg #2, 3 | 396.4* | 2955.2* | 5.90E-05* | Theis |
| Gragg #2, 3 | 426.7 | 3191.9 | 4.63E-05 | Cooper-Jacob |
| Avg | 354.3 | 2650.5 | 4.5E-05 | |
| Gragg #3 Pumping Wel | 1 | | | |
| Gragg #3 Pumping | 100.3 | 750.3 | 8.18E-03 | Cooper-Jacob |
| Gragg #1 Obs | 475.5 | 3557.0 | 6.80E-04 | Theis |
| Gragg #1 Obs | 485.6 | 3632.5 | 4.75E-04 | Cooper- Jacob |
| Gragg #2 Obs | 721.1 | 5394.2 | 1.10E-04 | Theis |
| Gragg #2 Obs | 487.3 | 3645.3 | 1.67E-04 | Cooper- Jacob |
| Gragg # 1, 2, 3 | 153.3 | 1146.8 | 5.12E-05 | Theis |
| Gragg # 1, 2, 3 | 129.2 | 966.5 | 4.59E-04 | Cooper-Jacob |

Table 5. Results of parameter estimation of all wells.

| Well Name | T (ft2/day) | T (gpd/ft2) | S | Analytical Solution | | | |
|------------------------------------------|----------------|----------------|----------|---------------------|--|--|--|
| Gragg #1, 2 Obs | 441.6 | 3303.4 | 2.55E-04 | Theis | | | |
| Gragg #1, 2 Obs | 705.9 | 5280.5 | 3.12E-04 | Cooper-Jacob | | | |
| Gragg #2, 3 | 691.0 | 5169.0 | 1.07E-04 | Theis | | | |
| Gragg #2, 3 | 583.2 | 4362.6 | 1.39E-04 | Cooper-Jacob | | | |
| Avg | 487.4 | 3151.0 | 2.76E-04 | | | | |
| Gragg #1 Pumping (2018 Single Well Test) | | | | | | | |
| Gragg #1 Pumping | 165.7 | 1239.5 | 2.99E-15 | Theis | | | |
| *1 | | | | | | | |

*best fit values

Table 6. Aquifer and Trinity well parameters calculated from data collected during the pumping and recovery phase of the aquifer test. These values were used in analytical modeling forecasts.

| Specific | Storativity | Tra | ansmissivity (T) ft ² /day | |
|-------------------------|-------------|--------------|---------------------------------------|---------|
| (gpm ft ⁻¹) | (S) | Theis (1963) | Cooper-Jacob (1946) | Average |
| 0.5 | 5.57-E05* | 399* | 403 | 401 |

*average of best fit values

DRAWDOWN FORECASTING

This memo documents an aquifer test that could be used as a component of the hydrogeologic report of an application for a pumping permit. District rules require any application for a pumping permit to have an evaluation (hydrogeologic report) of the potential for unreasonable impacts from the proposed pumping (BSEACD, 2016). An important part of that evaluation is using aquifer test data to estimate aquifer parameters to make forecasts of the potential range of drawdown into the future. This report uses those aquifer parameters and the assumed pumping rate to make some estimates of drawdown. For purposes of this evaluation we assume a potential request of about 200 million gallons per year, which is the equivalent to 380 gpm, or about 130 gpm for each of the three wells in the well field. This report does not constitute an evaluation of the potential for unreasonable impacts.

A simple estimate of drawdown from parameters in **Table 6** is presented in **Figure 10**. Results presented show an approximation of drawdown after 4 days of pumping from a hypothetical well in the well field at a rate of 380 gpm. Drawdown is estimated to be a total of 265 ft in the pumping well with drawdown decreasing to 0 ft at a distance of 8,930 ft from the well (**Figure 10**). Using the same parameters when time is increased to 30 years, a total estimated drawdown of 380 ft within the pumping well decreases to about 112 ft at a distance of 10,000 ft radial from the pumping well (**Figure 10**).

Aqtesolv allows a more sophisticated forward modeling and geographic drawdown estimation using all three wells and the parameters in **Table 6**. Figure 11 presents a 30-year average drawdown. All three wells

collectively pumping at 380 gpm resulted in a combined drawdown of about 140 ft at a radial distance of about 10,000 ft from the well field.



Figure 10. Four-day and thirty-year theoretical drawdown versus distance of the Lower Trinity well modeled using (Cooper and Jacob, 1946).



Figure 11. *Map of combined drawdown from pumping 200 MGD (380 gpm) after 30 years using Aqtesolv and the Theis solution.*

Water Quality

Physicochemical data of the groundwater produced from Gragg #2 and #3 was measured throughout both tests with a Horiba water-quality instrument. Temperature, pH, conductivity, and dissolved oxygen values did not vary greatly between probe readings (**Table 7**). Water samples were collected at the termination of pumping for Gragg #1 (8/28/2019), Gragg #2 (10/22/19), and Gragg #3 (10/28/19) and submitted for laboratory analyses at LCRA Environmental Laboratory Services (**Table 8**; **Appendix E**). Ion geochemistry indicates Ca-HCO₃ water with relatively low TDS (542-568 mg/L) and sulfate (161-169 mg/L). All other water-quality parameters analyzed were within ranges characteristic of the Lower Trinity Aquifer. These results indicate that the water in the Lower Trinity Aquifer likely meets the TCEQ's primary and secondary public drinking water standards. Isotope data was collected from Gragg #1 at the end of its single pumping test. Isotope results indicate very low tritium (-0.05 TU) and carbon-14 (0.006 PMC), indicating very old (pre-modern) water (**Appendix F**).

Table 7. Physicochemical well-water data monitored during pumping of both Lower Trinity wells with a Horiba water-quality probe. Values did not vary greatly between readings and were found to be within ranges characteristic of the Lower Trinity Aquifer.

| Event | Temp (°C) | pН | Conductivity (µs/cm) | DO (mg/L) |
|----------|-----------|------|----------------------|-----------|
| Gragg #2 | 29.61 | 7.49 | 908 | 5.38 |
| Gragg #3 | 30.09 | 7.29 | 906 | 6.45 |

| Table 8. | Gragg | #1 -3 L | ower | Trinity | groundwate | r sample | results | processed b | y LCRA |
|----------|----------|----------------|--------|----------|------------|----------|---------|-------------|--------|
| Environ | mental . | Labora | tory S | Services | 5. | | | | |

| | Gragg #1 | Gragg #2 | Gragg #3 |
|------------------------|----------|----------|----------|
| Parameter | Result | Result | Result |
| Hardness (mg/L) | 196 | 184 | 162 |
| Calcium Total (mg/L) | 78.3 | 73.8 | 65.0 |
| Iron Total (mg/L) | 0.431 | 0.497 | 0.217 |
| Sodium Total (mg/L) | 32.5 | 43.5 | 76.0 |
| Aluminum Total (mg/L) | 0.0099 | 1.06 | < 0.0050 |
| Arsenic Total (mg/L) | < 0.0010 | <0.0010 | < 0.0010 |
| Copper Total (mg/L) | 0.0017 | < 0.0010 | 0.0017 |
| Lead Total (mg/L) | 0.0007 | 0.0022 | < 0.0010 |
| Manganese Total (mg/L) | 0.0044 | 0.0066 | 0.00519 |
| Zinc Total (mg/L) | 0.327 | 0.352 | 0.399 |
| Chloride (mg/L) | 19 | 32.8 | 45.9 |
| Fluoride (mg/L) | 1.85 | 1.67 | 1.80 |
| Alkalinity (mg/L) | 254 | 259 | 249 |

| | Gragg #1 | Gragg #2 | Gragg #3 |
|------------------------|----------|----------|----------|
| Nitrate/Nitrite (mg/L) | < 0.020 | < 0.010 | < 0.010 |
| Sulfate (mg/L) | 162 | 161 | 169 |
| TDS (mg/L) | 542 | 559 | 568 |
| Total Coliform | N/A | Absent | Absent |
| Ecoli | N/A | Absent | Absent |
| Isotopes | | | |
| Sr 87/86 (Ratio) | 0.708372 | N/A | N/A |
| Deut./O18 (VSMOW) | -24.6 | N/A | N/A |
| Tritium (TU) | -0.05 | N/A | N/A |
| Carbon-14 (Y-BP) | 41100 | N/A | N/A |

CONCLUSIONS

Because the results of the aquifer test indicate that the water quality and yield of these wells are high the Lower Trinity Aquifer may be a direct alternative groundwater supply for the study area. At this time there are no large permitted Lower Trinity wells in the BSEACD.

However, further evaluation of the Lower Trinity is needed to determine how long-term pumping from the Lower Trinity could affect water levels (storage) over time and space. The nearby Lower Trinity Aquifer of western Travis County offers a cautionary example of groundwater mining (Hunt et al., 2020).

In addition, the Lower Trinity Aquifer could be a good candidate for ASR. However, more study is needed to evaluate its ASR potential.

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APPENDIX A: State well reports

| | STAT | TE OF TEXA | S WELL REI | PORT for Tra | acking #473734 |
|------------------------------------------------------------------------------------------------------------|-----------------------------------|------------------------------------------------------------------------------------------|-----------------------------|-----------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------|
| Owner: | Gragg |) Tract, LP | | Owner Well #: | 1 |
| Address: | 1010 V | N. Martin Luther H | King Jr. Blvd. | Grid #: | 58-50-7 |
| Well Location: | Old Bl | liss Spillar Rd. | | Latitude: | 30° 08' 05.03" N |
| | Manch | naca, TX 78652 | | Longitude: | 097° 52' 00.85" W |
| Well County: | Hays | | | Elevation: | 742 ft. above sea level |
| Type of Work: | New W | /ell | | Proposed Use | Public Supply |
| Drilling Start Date | e: 10/3 | 0/2017 Drilling | g End Date: 1/26/ | 2018 | Plans Approved by TCEQ |
| | [| Diameter (in. |) Tr | op Depth (it.) | Bottom Depth (ft.) |
| Borehole: | | 13.5 | | 0 | 1400 |
| | | 8 | | 1400 | 1620 |
| Drilling Method: | | Air Rotary | | | |
| Borehole Comple | etion: | Perforated or Sk | otted | | |
| | [| Top Depth (ft.) | Bottom Depth (ft. |) Descr | ption (number of sacks & material) |
| | | 0 | 1342 | C | ement 1175 Bags/Sacks |
| Annular Seal Dat | ta: | • | | | |
| Annular Seal Dat Seal Meth | ta: od: Po: | sitive Displaceme | nt | Distance to Prop | erty Line (ft.): No Data |
| Annular Seal Dat Seal Meth Sealed I | ta: od: Po: By: Dri | sitive Displaceme ller | nt C | Distance to Prop Distance to Septic I concentrated conta | erty Line (ft.): No Data Field or other mination (ft.): none |
| Annular Seal Dat Seal Meth Sealed I | ta: od: Po: By: Dri | sitive Displaceme ller | nt C | Distance to Prop Distance to Septic Concentrated conta Distance to Se | erty Line (fL): No Data Field or other Imination (fL): none ptic Tank (fL): none |
| Annular Seal Dat Seal Meth Sealed I | ta: od: Po: By: Dri | sitive Displaceme ller | ent C | Distance to Prop Distance to Septic l concentrated conta Distance to Se Method o | erty Line (ft.): No Data Field or other mination (ft.): none ptic Tank (ft.): none of Verification: No Data |
| Annular Seal Dat Seal Meth Sealed I Surface Completi | ta: od: Po: By: Dri ion: | sitive Displaceme ller Surface Slab Ins | nt C talled | Distance to Prop Distance to Septic I concentrated conta Distance to Se Method o Surf | erty Line (fL): No Data Field or other Imination (fL): none ptic Tank (fL): none of Verification: No Data face Completion by Driller |
| Annular Seal Dat Seal Meth Sealed I Surface Completi Water Level: | ta: od: Po: By: Dri ion: | sitive Displaceme ller Surface Slab Ins 196 ft. below lan | talled d surface on 2018 | Distance to Prop Distance to Septic I concentrated conta Distance to Se Method o Surf 8-01-08 | erty Line (ft.): No Data Field or other amination (ft.): none ptic Tank (ft.): none of Verification: No Data face Completion by Driller |
| Annular Seal Dat Seal Meth Sealed i Surface Completi Water Level: Packers: | ia: od: Po: By: Dri ion: | sitive Displaceme ller Surface Slab Ins 196 ft. below lan No Data | talled | Distance to Prop Distance to Septic I concentrated conta Distance to Se Method o Surf 8-01-08 | erty Line (ft.): No Data Field or other imination (ft.): none ptic Tank (ft.): none of Verification: No Data face Completion by Driller |
| Annular Seal Dat Seal Meth Sealed I Surface Completi Water Level: Packers: Type of Pump: | ta: od: Po: By: Dri ion: | sitive Displaceme ller Surface Slab Ins 196 ft. below lan No Data No Data | talled | Distance to Prop Distance to Septic l concentrated conta Distance to Se Method o Surf 8-01-08 | erty Line (ft.): No Data Field or other mination (ft.): none ptic Tank (ft.): none of Verification: No Data face Completion by Driller |

Well Report Tracking Number 473734 Submitted on: 3/27/2018 Page 1 of 3

| Water Quality: | 1434 - 1620 | Trinity | | |
|----------------------|----------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------|-----------------------------------------------------------|
| | | Chemical Analysis Made | Yes | |
| | Did the driller know | wingly penetrate any strata which contained injurious constituents? | : No | |
| Certification Data: | The driller certified that the driller's direct supervision correct. The driller under the report(s) being return | he driller drilled this well (or the wo n) and that each and all of the stat rstood that failure to complete the red for completion and resubmitta | ell was dril ements he required it I. | led under the rein are true and tems will result in |
| Company Information: | Bee Cave Drilling, Inc | | | |
| | 185 Angel Fire Dr. Dripping Springs, TX | 78620 | | |
| Driller Name: | Jim Blair | License | Number: | 54416 |
| Comments: | From Geologging: Georgetown Edwards Edwards 100' - 430' Walnut Edwards 430' | - 460' | | |

| DESCRIPT | TION & COL | Lithology: OR OF FORMATION MATERIAL |
|-----------|--------------|----------------------------------------------|
| Top (ft.) | Bottom (ft.) | Description |
| 0 | 2 | topsoil |
| 2 | 12 | caliche |
| 12 | 32 | tan & white broken limestone |
| 32 | 390 | Edwards Limestone w/ voids (lost returns) |
| 390 | 1085 | no returns |
| 1085 | 1090 | gray limestone |
| 1090 | 1130 | gray sandstone |
| 1130 | 1165 | gray limestone |
| 1165 | 1200 | gray sandstone |
| 1200 | 1270 | brown & gray limestone |
| 1270 | 1350 | gray limestone |
| 1350 | 1620 | gray sandstone & limestone |

| BLANK I | Casing PIPE & WELL | SCREEN | DATA | |
|---------|-----------------------|--------|------|--|
| | | | | |

| Dia (in.) | Туре | Material | Sch./Gage | Top (ft.) | Bottom (ft.) |
|--------------|--------------------------|----------------------|-----------|-----------|-----------------|
| 8 | Blank | New Steel | sch. 40 | 0 | 1342 |
| 5 | Blank | New Plastic (PVC) | sch. 80 | 1334 | 1434 |
| 5 | Perforated or Slotted | New Plastic (PVC) | sch. 80 | 1434 | 1614 |

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| | STATE O | FTEXAS | S WELL R | EPORT for Tr | acking #527500 | |
|---------------------|----------------------------------------------------------|----------------------|-----------------------------------------------------------------------------------|--------------------|-------------------------------------|----------|
| Owner: | Gragg Tract | LP #2 | | Owner Well # | t 2 | |
| Address: | 1010 W. Mart Austin, TX 7 | in Luther K 8701 | King Jr. Blvd. | Grid #: | 58-50-7 | |
| Well Location: | Old Bliss Spi Manchaca, T | illar Rd. X 78652 | | Latitude: | 30° 07' 53.46" N | |
| Well County: | Hays | | | Elevation: | 732 ft. above sea leve | 4 |
| Type of Work: | New Well | | | Proposed Us | e: Public Supply | |
| Drilling Start Date | : 8/22/2019 | Drilling | End Date: 9/ | 25/2019 | Plans Approved by T | CEQ - NO |
| | | Diameter (in.) |) | Top Depth (ft.) | Bottom Depth (ft.) | |
| Borehole: | | 15 | | 0 | 20 | |
| | | 12.75 | | 20 | 1505 | |
| | | 7.875 | | 1505 | 1700 | |
| Drilling Method: | Air Ro | otary | | | | |
| Borehole Complet | tion: Open | Hole | | | | |
| | Тор | Depth (ft.) | Bottom Dept | h (ft.) Desc | ription (number of sacks & material |) |
| Annular Seal Data | a: | 0 | 1350 | C | ement 1148 Bags/Sacks | |
| Seal Metho | d: Positive D |)isplaceme | nt | Distance to Pro | perty Line (ft.): 220 | |
| Sealed B | Seal Method: Positive Displacement Sealed By: Driller | | Distance to Septic Field or other concentrated contamination (fL): none | | | |
| | | | | Distance to S | eptic Tank (ft.): none | |
| | | | | Method | of Verification: No Data | |
| Surface Completion | on: Surfac | æ Slab Inst | talled | Su | face Completion by Driller | r |
| Water Level: | 136 f | t. below lan | d surface on 2 | 2019-10-18 | | |
| Packers: | No Da | ata | | | | |
| Type of Pump: | No Da | ata | | | | |
| Well Tests: | Pump | | Yield: 17 | 0 GPM with 425 ft. | drawdown after 96 hours | |

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| | Strata Depth (ft.) | Water Type | |
|----------------------|---------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------|
| Water Quality: | No Data | No Data | |
| | | Chemical Analysis Made | Yes |
| | Did the driller know | vingly penetrate any strata which contained injurious constituents? | No |
| Certification Data: | The driller certified that th driller's direct supervision correct. The driller under the report(s) being return | e driller drilled this well (or the we) and that each and all of the stat stood that failure to complete the ed for completion and resubmittal | ell was drilled under the ements herein are true and required items will result in |
| Company Information: | : Bee Cave Drilling, Inc. 185 Angel Fire Dr. | | |
| | 185 Angel Fire Dr. Dripping Springs, TX | 78620 | |
| Driller Name: | Jim Blair | License | Number: 54416 |
| Comments: | Cementing by CUDD F | Pumping Services using Type H | I Cement per BSEACD |
| Li | thology: | | Casing: |
| | | | |

Bottom Dla Description Top (ft.) Bottom (ft.) Туре Material Sch./Gage Top (ft.) (In.) (ft.) 0 2 topsoil 8.625 Blank New Steel 0 1350 sch, 40 2 20 tan limestone 20 45 white limestone 45 80 tan limestone 80 140 lost returns 140 280 tan sandstone 280 300 gravel 300 340 tan sandstone & gravel 340 1700 lost returns

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

TEX. OCC. CODE Title 12, Chapter 1901.251, authorizes the owner (owner or the person for whom the well was drilled) to keep information in Well Reports confidential. The Department shall hold the contents of the well log confidential and not a matter of public record if it receives, by certified mail, a written request to do so from the owner.

Please include the report's Tracking Number on your written request.

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| SI | ATE OF TEXAS | S WELL REPO | ORT for Tra | cking #527505 | |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------|
| Owner: Gra | agg Tract LP #3 | | Owner Well #: | 3 | |
| Address: 101 | IO W. MLK Jr. Blvd. | | Grid #: | 58-50-7 | |
| Au: | Sun, IA 76701 | | Latitude: | 30° 07' 51.92" N | |
| Ma | nchaca, TX 78652 | | Longitude: | 097° 51' 41.78" W | |
| Well County: Hay | ys | | Elevation: | 722 ft. above sea level | |
| Type of Work: New | v Well | | Proposed Use: | Public Supply | |
| Drilling Start Date: 9 | /5/2019 Drilling | g End Date: 10/10/20 |)19 | Plans Approved by TCE | Q - NC |
| | Diameter (in. |) Top [| Pepth (fl.) | Bottom Depth (ft.) | |
| Borehole: | 15 | | 0 | 19 | |
| | 12.75 | | 19 | 1385 | |
| | 7.875 | 1 | 385 | 1700 | |
| Drilling Method: | Air Rotary | | | | |
| Drilling Method: Borehole Completion | Air Rotary | | | | |
| Drilling Method: Borehole Completion | Air Rotary Open Hole Top Depth (ft.) | Bottom Depth (fL) | Descrip | tion (number of sacks & material) | |
| Drilling Method: Borehole Completion Annular Seal Data: | Air Rotary c Open Hole Top Depth (ft.) 0 | Bottom Depth (fL) 1355 | Descrip | tion (number of sacks & material) ment 1195 Bags/Sacks | |
| Drilling Method: Borehole Completion Annular Seal Data: Seal Method: I | Air Rotary : Open Hole Top Depth (nt.) 0 Positive Displaceme | Bottom Depth (it.) 1355 ant D | Descrip Cer listance to Prope | tion (number of sacks & material) ment 1195 Bags/Sacks erty Line (ft.): 150 | |
| Drilling Method: Borehole Completion Annular Seal Data: Seal Method: Sealed By: | Air Rotary C Open Hole Top Depth (ft.) 0 Positive Displaceme Driller | Bottom Depth (ft.) 1355 ent Dist con | Descrip Cer listance to Prope ance to Septic F centrated contar | tion (number of sacks & material) ment 1195 Bags/Sacks erty Line (fL): 150 ield or other mination (fL): none | |
| Drilling Method: Borehole Completion Annular Seal Data: Seal Method: I Sealed By: I | Air Rotary : Open Hole Top Depth (ft.) 0 Positive Displaceme Driller | Bottom Depth (ft.) 1355 ent Dist con | Descrip Cer Distance to Prope ance to Septic F centrated contar Distance to Sep | oton (number of sacks & material) ment 1195 Bags/Sacks erty Line (ft.): 150 ield or other mination (ft.): none stic Tank (ft.): none | |
| Drilling Method: Borehole Completion Annular Seal Data: Seal Method: Sealed By: I | Air Rotary : Open Hole Top Depth (IT.) 0 Positive Displaceme Driller | Bottom Depth (ft.) 1355 ent Dist con | Descrip Cer listance to Prope ance to Septic F centrated contar Distance to Sep Method of | ton (number of sacks & material) ment 1195 Bags/Sacks erty Line (ft.): 150 ield or other mination (ft.): none stic Tank (ft.): none f Verification: No Data | |
| Drilling Method: Borehole Completion Annular Seal Data: Seal Method: I Sealed By: I Surface Completion: | Air Rotary : Open Hole Top Depth (ft.) 0 Positive Displaceme Driller Surface Slab Inst | Bottom Depth (ft.) 1355 ent Dist con | Descrip Cer Distance to Prope ance to Septic F centrated contar Distance to Sep Method of Surfa | nton (number of sacks & material) ment 1195 Bags/Sacks erty Line (fL): 150 ield or other mination (fL): none otic Tank (fL): none f Verification: No Data ace Completion by Driller | |
| Drilling Method: Borehole Completion Annular Seal Data: Seal Method: Sealed By: Surface Completion: Water Level: | Air Rotary : Open Hole Top Depth (ft.) 0 Positive Displaceme Driller Surface Slab Inst 132 ft. below lan | Bottom Depth (ft.) 1355 ent Dist con talled | Descrip Cer Distance to Prope ance to Septic F centrated contar Distance to Sep Method of Surfa | nton (number of sacks & material) ment 1195 Bags/Sacks erty Line (fL): 150 ield or other mination (fL): none otic Tank (fL): none f Verification: No Data ace Completion by Driller | |
| Drilling Method: Borehole Completion Annular Seal Data: Seal Method: I Sealed By: I Surface Completion: Water Level: Packers: | Air Rotary : Open Hole Top Depth (IT.) 0 Positive Displaceme Driller Surface Slab Inst 132 ft. below lan No Data | Bottom Depth (ft.) 1355 ent Dist con talled d surface on 2019-1 | Descrip Cer Distance to Prope ance to Septic F centrated contar Distance to Sep Method of Surfa | ton (number of sacks & material) ment 1195 Bags/Sacks erty Line (ft.): 150 ield or other mination (ft.): none otic Tank (ft.): none f Verification: No Data ace Completion by Driller | |
| Drilling Method: Borehole Completion Annular Seal Data: Seal Method: Sealed By: Surface Completion: Water Level: Packers: Type of Pump: | Air Rotary Copen Hole Top Depth (ft.) O Positive Displaceme Driller Surface Slab Inst 132 ft. below lan No Data No Data | Bottom Depth (ft.) 1355 ent Dist con talled d surface on 2019-1 | Descrip Cer Vistance to Prope ance to Septic F centrated contar Distance to Sep Method of Surfa | ton (number of sacks & material) ment 1195 Bags/Sacks erty Line (ft.): 150 ield or other mination (ft.): none stic Tank (ft.): none f Verification: No Data ace Completion by Driller | |

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| | Strata Depth (it.) | Water Type | | |
|----------------------|-----------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------|------------------------------------------------------------|
| Water Quality: | No Data | No Data | | |
| | | Chemical Analysis Made | Yes | |
| | Did the driller kno | owingly penetrate any strata which contained injurious constituents? | No | |
| Certification Data: | The driller certified that driller's direct supervisio correct. The driller under the report(s) being return | the driller drilled this well (or the we on) and that each and all of the stat erstood that failure to complete the med for completion and resubmittal | ell was dril ements he required i | led under the erein are true and tems will result in |
| Company Information: | Bee Cave Drilling, In | c. | | |
| | 185 Angel Fire Dr. Dripping Springs, TX | 78620 | | |
| Driller Name: | Jim Blair | License | Number: | 54416 |
| Comments: | Cementing by CUDD | Pumping Services using Type H | l Cement | per BSEACD |
| | | | | |

DESCRIPTION & COLOR OF FORMATION MATERIAL

Casing: BLANK PIPE & WELL SCREEN DATA

| Top (ft.) | Bottom (ft.) | Description | Dla (In.) | Туре | Material | Sch./Gage | Top (ft.) | Bottom (ft.) |
|-----------|--------------|------------------------|--------------|-------|-----------|-----------|-----------|-----------------|
| 0 | 5 | topsoil | 8.625 | Blank | New Steel | sch. 40 | 0 | 1355 |
| 5 | 140 | tan limestone | | | | | | |
| 140 | 290 | tan limestone & gravel | | | | | | |
| 290 | 1700 | lost returns | | | | | | |
| 1300 | 1350 | Hammett | | | | | | |
| 1350 | 1425 | Sligo | | | | | | |
| 1425 | 1700 | Hosston | | | | | | |

IMPORTANT NOTICE FOR PERSONS HAVING WELLS DRILLED CONCERNING CONFIDENTIALITY

TEX. OCC. CODE Title 12, Chapter 1901.251, authorizes the owner (owner or the person for whom the well was drilled) to keep information in Well Reports confidential. The Department shall hold the contents of the well log confidential and not a matter of public record if it receives, by certified mail, a written request to do so from the owner.

Please include the report's Tracking Number on your written request.

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| | | | | | | | nments: | Cor |
|----------------------------|-----------------------------------|------------------------|---------------------|----------|--------|-----------|--------------------------------|---------|
| 20 | 40 | 1613' | 35 | | - | | IPER | CA |
| 20 | - 166 | 1612' | 35 | * | N | | SISTIVITY, SP | RE |
| . 20 | 28 | 1606' | 35 | ÷ | N | 3 | MMA | /D 2 |
|) FT./ IN. |) TO (ft | FROM (ft) | D (ft/min) | SPEE | NO | RUN | TYPE | LOG |
| | | | | | | els | eu by - Kelly ess: John Mik | With |
| Ō | nit/Truck- (| = | | OUNCE IN | | T | | - |
| | | Deg C | at: | GENER | Rm: | | sity: | Visco |
| rc: | te Since Ci | Tim | e: | ud Type | M | | Medium: | Hole |
| (ft) : 196' | uid Level | Ш | | ight: | We | ROTARY | Nethod: AIR F | Drill N |
| | | 1 | | | | | | ω |
| | 4 | 3 | (k) | 620' | | 1402' | 7 7/8" | N |
| 1343' | 1.9' | + | 8" Steel | 1402' | 8 | Q | . 13.5" | - |
| TO (ft) | OM (ft) | HK FR | SIZE/WGT/T | (Ħ) | ТО | -ROM (ft) | BIT SIZE (in) | RUN |
| םר | ING RECOR | CAS | | | | RECORD | BIT | |
| 018 | 01-08-2 | e Drilled: | Dat | | | | n Ref: G.L. | Dept |
| | (ft):1614' | ger T.D. | Log | | | S | tion: 723' GP | Eleva |
| | (ft) : 1620' | er T.D. (| Drill | BOREHO | < m | BEE CA | ng Contractor: | Drilli |
| | TX | State: | 5 | 7.8669 | ×-9 | 30.13469 | tion: N | Loca |
| | : HAYS | County | | | | ΥE | It: BEE CA | Clier |
| 18 | 01-08-20 | Date: | WELL | RACK | 3G TI | S - GRA | ct: WALTER | Proje |
| 10-495-9121 | N | (78217 | an Antonio, T) | Rd. Sa | assen | 17118 CI | Cam, Inc. | Geo |
| STIVITY, P., STIVITY | MA, RESIS PER, TEM D CONDUC | GAMI CALII FLUII | Logs: I Services | ording |) Rec | g & Video | r Well Loggin | Wate |
| K TEST WELL | AGG TRAC | e: GR/ | Borehol | | | J | í / / / | |
| | | | | | | | | |

APPENDIX B: Geophysical Logs (Wells 1, 2, & 3 respectively)

| SPR | | Depth | | N16 | | _ | Caliper | |
|-------|-----|----------|---|-------|-----|---|-----------------------------|----------|
| Ohm | 125 | 1in:20ft | 0 | Ohm m | 250 | 2 | IN | 22 |
| Gamma | | | | N64 | 200 | _ | 8 1/2 Inch Bit Mark | |
| CPS | 100 | | | 1104 | | 2 | | 22 |
| SPR#2 | | | 0 | Ohm.m | 250 | | 7 3/4 Inch Bit Mark | |
| | 125 | | | N8 | | 2 | | 22 |
| | | • | 0 | Ohm.m | 250 | | Wash Out 7 3/4 Inch Bit Mar | (|
| | | | | N32 | | | | |
| | | | 0 | Ohm.m | 250 | | Wash Out 8 1/2 Inch Bit Mar | (|

WALTERS - GRAGG TRACK WELL

0

0

0

| | N64#1 | | | Caliper#1 | |
|---|-------|-----|---|-----------------------------|------|
| 0 | Ohm.m | 250 | 2 | In | 22 |
| | N8#1 | | | 7 7/8 Inch Bit Mark | |
| 0 | Ohm.m | 250 | 2 | | 22 |
| | N16#2 | | | 13.5 Inch Bit Mark | |
| 0 | Ohm.m | 200 | 2 | | 22 |
| | N32#2 | | | Wash Out 7 7/8 Inch Bit Ma | ark |
| 0 | Ohm.m | 200 | | | |
| | | | | Wash Out 13 1/2 Inch Bit M | lark |
| | | | | | |
| | | | | Under Cut 13 1/2 Inch Bit N | lark |

22

7 7/8 Inch Bit Mark#1

















| • | \mathbf{r} | www.well-scope.com 512-798-1888 | | | | | |
|-----------------------------|------------------------|------------------------------------|-------------|------------------|--|--|--|
| WY ALI | scops | Borehole: | Bliss S | pillar #2 | | | |
| DRIPPING GEOPHYSICAL LOG | SPRINGS, TEXAS | Logs: | Gam, I | Res, SP, SPR, Ca | | | |
| PO Box 572, Drip | ping Springs, TX 78620 | | | | | | |
| Project: | Bliss Spillar | - | Date: | 08/30/2019 | | | |
| Client: | Bee Cave Drilling | | County: | Hays | | | |
| Location: | 30.1315 -97.8680 | | State: | ТХ | | | |
| | Boreho | ole Data | | | | | |
| Contractor: | Bee Cave Drilling | Dri | lled TD (ft |): 1505' | | | |
| | | · · · · · · | / | | | | |

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| BIT SIZE (in) 15" 12 5/8" ethod: Ai | FROM (ft 0 20 | t) | TO (ft) | SIZE | E/WGT/THK | FROM (ff) | | | | |
| 15" 12 5/8" :thod: _Ai | 0 20 | | 20 | | | | 10 (ft) | | | |
| 12 5/8" :thod: Ai | 20 | | 20 | 14" | steel | +1 | 19' | | | |
| thod: Ai | | | 1505' | | | | | | | |
| | r Rotary | | Weight | t: | Flu | uid Lvl (ft): | 130' | | | |
| edium:Ro | ock/clay | | Mud Ty | pe: | foam | Circ Time: | 1hr | | | |
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| <u>General Data</u> | | | | | | | | | | |
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| s: Mi | ke Scott | | | | | | | | | |
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| | 2 | 20 | | | 1500' | 5 | ft | | | |
| | 1 | 30 | | | 1505' | 3' | ft | | | |
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| | SCOP SPRINGS, TEXAS | Boreho Logs: | 512-798-10 Die: Bliss S Gam, I | 888 Spillar #3 Res, SP, SPR |
| DRIPPING BEOPHYSICAL LOG PO Box 572, Drid | SCOP SPRINGS, TEXAS SGING & CAMERA SERVIT Oping Springs, TX 786 | Boreho Logs: | 512-798-16 Die: Bliss S Gam, I | 888 Spillar #3 Res, SP, SPR |
| DRIPPING BEOPHYSICAL LOG PO Box 572, Drip Project: | SPRINGS, TEXAS SGING & CAMERA SERVIT Oping Springs, TX 786 Bliss Spillar | Boreho Logs: | 512-798-14 Die: Bliss S Gam, f | 888 Spillar #3 Res, SP, SPR 09/11/2019 |
| DRIPPING GEOPHYSICAL LOG PO Box 572, Drip Project: Client: | SPRINGS, TEXAS SPRINGS, TEXAS SGING & CAMERA SERVIT Oping Springs, TX 786 Bliss Spillar Bee Cave Drilling | Boreho Logs: 20 | 512-798-18 Die: Bliss S Gam, Bliss S Bliss S Gam, Bliss S Gam, Bliss S Bliss S Bliss S Bliss S Bliss S Bliss S Bliss S Gam, Bliss S Bliss S Blis | 888 Spillar #3 Res, SP, SPR 09/11/2019 Hays |
| DRIPPING DRIPPING DEOPHYSICAL LOG PO Box 572, Drip Project: Client: Location: | SPRINGS, TEXAS SGING & CAMERA SERVIT Oping Springs, TX 786 Bliss Spillar Bee Cave Drilling 30.1310 -97.861 | Boreho Logs: 20 | 512-798-10 Die: Bliss S Gam, 1 Date: County: State: | 888 Spillar #3 Res, SP, SPR 09/11/2019 Hays TX |
| DRIPPING GEOPHYSICAL LOG PO Box 572, Drip Project: Client: Location: | SPRINGS, TEXAS SPRINGS, TEXAS SGING & CAMERA SERVIT Pping Springs, TX 786 Bliss Spillar Bee Cave Drilling 30.1310 -97.8612 | Boreho Logs: 20 5 Borehole Data | 512-798-18 Dle: Bliss S Gam, Bliss S Gam, Bliss S County: State: | 888 Spillar #3 Res, SP, SPR 09/11/2019 Hays TX |
| DRIPPING SEOPHYSICAL LOG PO Box 572, Drip Project: Client: Location: Contractor: | SPRINGS, TEXAS SPRINGS, TEXAS SGING & CAMERA SERVIT Diping Springs, TX 786 Bliss Spillar Bee Cave Drilling 30.1310 -97.861 Bee Cave Drilling | Boreho Logs: 20 | 512-798-10 Die: Bliss S Gam, f Date: County: State: Drilled TD (ff | 888 Spillar #3 Res, SP, SPR 09/11/2019 Hays TX TX |
| DRIPPING DEOPHYSICAL LOG PO Box 572, Drip Project: Client: Location: Contractor: Elevation: | SCOP SPRINGS, TEXAS GING & CAMERA SERVIN Oping Springs, TX 786 Bliss Spillar Bee Cave Drilling 30.1310 -97.861 Bee Cave Drilling Bee Cave Drilling | Boreho Logs: 20 | 512-798-10 Die: Bliss S Gam, I Date: County: State: Drilled TD (fi Logged TD (| 888 Cipillar #3 Res, SP, SPR 09/11/2019 Hays TX TX t): 1535' ft): 1531' |

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APPENDIX C: Well Schematics (Wells #1 and #3)

Schematic of Gragg #1 Lower Trinity Well construction and stratigraphy. Stratigraphic picks made from a geophysical log. Gragg #1 was used only as an observation well. Static water level is shown in ft-dtw.



Schematic of Gragg #3 well construction and stratigraphy with modeled water levels for 4-day and 30-yr pumping scenarios. Stratigraphic picks made from a geophysical log. Actual measured drawdown in well during #3 aquifer test was 460.8 ft-dtw.

APPENDIX D: Aquifer Test Work Plan



Proposed Work Plan for the Lower Trinity Aquifer Gragg Well Field, Hays County, Texas

October 8, 2019

The District proposes to support the collection of data from an aquifer test for the Lower Trinity Aquifer. The Lower Trinity Aquifer is presently an underutilized groundwater resource and may be an alternative water supply for the area. In addition, the Lower Trinity may be a good candidate for future Aquifer Storage and Recovery projects. The Aquifer Science Team views this testing as an important evaluation and characterization study. Few Lower Trinity Aquifer wells exist within the BSEACD and very little is known about the hydraulic properties of the aquifer. Leveraging the "well testing" that was planned as part of the drilling of the test wells, we suggest that the well owner (Bill Walters) and the District would both gain valuable information from a prolonged aquifer test following the District's Aquifer Test guidelines.

Aquifer Science staff propose to collect aquifer test data (continuous water levels), periodic water quality samples, and periodic pumping rate measurements during testing. This workplan would satisfy the District's Aquifer Test guidelines for a given volume tested.



Figure 1. Location of wells. Gragg #1 has a state well number 58-50-755.

Pumping Duration and Pumping Rate

This testing assumes that two wells, Gragg #2 and Gragg #3, will be pumped sequentially (not simultaneously). This test could be conducted to inform or support future production permit requests for this well field. The District issues permits for an annual volume that is based on nonspeculative demand estimates and aquifer testing evaluations. The well owner has indicated a potential future demand of 200 MGY from the Gragg well field, which is the assumed testing target for this test.

If this were a pumping permit request, the aquifer test would be designed to pump a minimum of three times the daily equivalent of the requested annual permitted volume. Given the target volume of 200 MGY and an assumed pumping rate of 150 gpm, each pumping well would need to be pumped for 96 hours (4 days) (**Table 1**).

 Table 1. Illustration showing how the duration of an aquifer test is determined from the requested permit amount and the pumping rate capacity of the pump.

| | Annual volume (gal) | Gal/d | Target Test Volume (3x Gal/d) |
|---------------|---------------------|---------|-------------------------------|
| | | | |
| Target volume | 200,000,000 | 547,945 | 1,643,836 |

| well | Estimated GPM | Pumping Time (hrs) | Test Volume/well (gallons) |
|---------|---------------|-----------------------|----------------------------|
| | | | - |
| Gragg 1 | | | |
| | | | |
| Gragg 2 | 150 | 96 | 864,000 |
| | | | |
| Gragg 3 | 150 | 96 | 864,000 |
| | - | Testhenest | · |

Test target

volume 1,728,000 gallons

*Assume 2 wells to be tested.

**estimated pumping rate of 150 gpm

The test will be a constant-rate test, which we assume to be pumped at a rate of about 150 gallons per minute based on communications with Kevin Langford of Bee Caves Drilling. Staff from the driller or Walters will be responsible for maintaining the pumping rate and duration within each well. In addition, recovery of the pumping well should reach 90% prior to removing the pump and starting the next testing phase (this is likely to be 4 to 6 hours based on Gragg #1).

The pumping rate will need to be measured periodically throughout the test, especially if a change in pumping rate is noted or the pump is adjusted. Measurements need to be made with a calibrated meter provided by the driller. The District may also make periodic flow measurements at the outflow to verify pumping rates.

The driller or Walters staff will also be responsible for containing or redirecting produced waters towards a beneficial purpose where possible (i.e. irrigating pastures, trees, landscapes).

Water-Level Data

Prior to the start of the test, District staff will install absolute (non-vented) pressure transducers in each of the two observation wells. A gauged (vented) pressure transducer with vented cable will be used in the pumping well. We assume a 1 inch tremie pipe will be installed in the pumping well to an adequate depth. District staff will collect data from the transducers periodically. The sample rate will be set at 1 minute for the pumping well, with observation wells set at a sample rate of a maximum of 15 minutes. Periodic manual measurements will be made throughout the testing.

After the aquifer testing, we would like to leave a pressure transducer within the Gragg #1 well to continue collecting water-level data. District staff would download the data quarterly.

Collecting the long-term data would not change the use or limit the well owner's future options for the well.

Water Quality

District staff will make periodic field measurements of temperature, conductivity, and pH during the test. At the start and end of pumping for each pumped well a sample will be collected and submitted to the lab for analysis of TDS. Other samples may be collected at differing time periods.

Communication and Access

District staff will need access to the site during normal working hours; overnight measurements will not be needed. District and driller or Walters staff will need to communicate actions and different activities such as start and stop of pumping, or other changes.

Data Delivery and Analyses

The data collected by the District will be in electronic form and will be provided to the well owner. The District will also analyze the data to calculate aquifer parameters and will document the results in a technical memorandum, which will also be made available to the well owner.

This aquifer-test data collection is a significant portion of the effort and expense required to perform an aquifer test that supports a production permit application. If this proposed test is conducted at a high rate of pumping for a sufficient period of time (**Table 1**), a later aquifer test will not be required for the permit application for this well field. If a permit application is made later, these data and results could be submitted as part of an overall hydrogeologic report submitted by a qualified geoscientist or engineer. The hydrogeologic report would need to follow the guidelines described in the District's Aquifer Test Guidelines.

Brian A. Smith, Ph.D., P.G.

Brian B. Hunt, P.G.

Vanessa Escobar

APPENDIX E: Water quality lab results (Wells #2 and #3)





LCRA Environmental Laboratory Services 3505 Montopolis Drive Austin, TX 78744 Phone: (512) 730-6022 Fax: (512) 730-6021

Analytical Results

| Lab ID: Q1973176001 | | Date R | eceived | 10/22/2 | 2019 1 | 6:09 | Ma | atrix: Drinking Wat | er | |
|--------------------------------|--------------------------|---------|----------|---------|--------|----------------|--------|---------------------|-----|-----|
| Sample ID: GRAGG 2 | | Date C | ollected | 10/22/2 | 2019 0 | 9:57 Sar | nple T | ype: SAMPLE | | |
| Project ID: NEW WELL BSEA | ACD | | | | | | | | | |
| | | | | | | | | | | |
| Parameter | Results Units | MRL | LOD | | DF | Prepared | Ву | Analyzed | Ву | Qua |
| ALKALINITY (SM2320B, Alkal | linity) | | | | | | | | | |
| Phenolphthalein Alkalinity | 0.00 mg/L | 0.00 | 0.00 | | 1 | | | 10/25/19 00:00 | ML | * |
| Hydroxide Alkalinity | 0.00 mg/L | 0.00 | 0.00 | | 1 | | | 10/25/19 00:00 | ML | |
| Bicarbonate Alkalinity | 259 mg/L | 0.00 | 0.00 | | 1 | | | 10/25/19 00:00 | ML | , |
| Carbonate Alkalinity | 0.00 mg/L | 0.00 | 0.00 | | 1 | | | 10/25/19 00:00 | ML | , |
| Total Alkalinity (CaCO3) | 259 mg/L | 20.0 | 20.0 | | 1 | | | 10/25/19 00:00 | ML | |
| INORGANICS (E200.7 Prep/E2 | 200.7 Metals, Trace Elen | nents) | | | | | | | | |
| Calcium Total | 73.8 mg/L | 0.200 | 0.0700 | | 1 | 10/24/19 11:08 | ME | 10/28/19 14:09 | FM | |
| Iron Total | 0.497 mg/L | 0.0500 | 0.0200 | | 1 | 10/24/19 11:08 | ME | 10/28/19 14:09 | FM | |
| Sodium Total | 43.5 mg/L | 0.200 | 0.0700 | | 1 | 10/24/19 11:08 | ME | 10/28/19 14:09 | FM | |
| INORGANICS (E200.8, ICP-MS | S Prep/E200.8, ICP-MS) | | | | | | | | | |
| Aluminum Total | 1.06 mg/L | 0.0500 | 0.0200 | | 10 | 10/24/19 11:17 | ME | 10/25/19 10:12 | FO | |
| Arsenic Total | <0.00100 mg/L | 0.00100 | 0.0004 | 0.01 | 1 | 10/24/19 11:17 | ME | 10/25/19 09:27 | FO | |
| Copper Total | <0.00100 mg/L | 0.00100 | 0 0004 | 1 | 1 | 10/24/19 11.17 | MF | 10/25/19 09:27 | FO | |
| Lead Total | 0.00216 mg/L | 0.00100 | 0 0004 | 0 015 | 1 | 10/24/19 11.17 | ME | 10/25/19 09:27 | FO | |
| Manganese Total | 0.00657 mg/l | 0.00100 | 0 0004 | 0.0.0 | 1 | 10/24/19 11:17 | ME | 10/25/19 09:27 | FO | |
| Zinc Total | 0.352 mg/L | 0.00500 | 0.0020 | | 1 | 10/24/19 11:17 | ME | 10/25/19 09:27 | FO | |
| INORGANICS (E2340B, Hardr | ness Calc.) | | | | | | | | | |
| Hardness, Calcium | 184 mg/L | | | | 1 | | | 10/28/19 15:26 | CW | |
| INORGANICS (E300.0, Anions | <i>;)</i> | | | | | | | | | |
| Chloride | 32.8 mg/L | 1.00 | 0.500 | | 1 | | | 10/23/19 09:51 | ML | |
| Fluoride | 1.67 mg/L | 0.0100 | 0.0050 | 4 | 1 | | | 10/23/19 09:51 | ML | |
| Nitrite (as N) | <0.0100 mg/L | 0.0100 | 0.0050 | 1 | 1 | | | 10/23/19 09:51 | ML | |
| Nitrate (as N) | <0.0100 mg/L | 0.0100 | 0.0050 | 10 | 1 | | | 10/23/19 09:51 | ML | |
| Sulfate | 161 mg/L | 5.00 | 2.50 | | 5 | | | 10/23/19 11:11 | ML | |
| TOTAL DISSOLVED SOLIDS (| SM2540C, TDS) | | | | | | | | | |
| Total Dissolved Solids(TDS) | 559 mg/L | 25.0 | 10.0 | | 10 | | | 10/25/19 11:01 | ERR | ! |
| Total Coliform by Colilert (SM | 19223, IDEXX) | | | | | | | | | |
| Residual Chlorine | <0.5 mg/L | | | | 1 | | | 10/22/19 16:29 | PJO | |
| Total Coliform | Absent P/A | 1.00 | 1.00 | | 1 | | | 10/22/19 16:29 | PJO | |
| Ecoli | Absent P/A | 1.00 | 1.00 | | 1 | | | 10/22/19 16:29 | PJO | |
| рН (SM4500-Н+В, рН @ 25&о | rdm;C) | | | | | | | | | |
| рН | 7.90 pH | 0.00 | 0.00 | | 1 | | | 10/25/19 08:04 | ML | |
| Temperature | 20.8 c | | | | 1 | | | 10/25/19 08:04 | ML | , |



LCRA Environmental Laboratory Services 3505 Montopolis Drive Austin, TX 78744 Phone: (512) 730-6021 Fax: (512) 730-6021

December 4, 2019

DANA WILSON BARTON SPRINGS - EDWARD AQUIFER CONSERVATION DISTRICT 1124 REGAL ROW AUSTIN, TX 78748

RE: Final Analytical Report Q1974421

Attn: DANA WILSON

Enclosed are the analytical results for sample(s) received by LCRA Environmental Laboratory Services. Results reported herein conform to the most current NELAP standards, where applicable, unless otherwise narrated in the body of the report. This final report provides results related only to the sample(s) as received for the above referenced work order.

Thank you for selecting ELS for your analytical needs. If you have any questions regarding this report, please contact us at (512) 730-6022. We look forward to assisting you again.

This report shall not be reproduced, except in full, and with written approval from LCRA Environmental Laboratory Services

Authorized for release by:

Dale funcha

Dale Jurecka Account Manager dale.jurecka@lcra.org



Enclosures:

Page 1 of 17



LCRA Environmental Laboratory Services 3505 Montopolis Drive Austin, TX 78744 Phone: (512) 730-6022 Fax: (512) 730-6021

Analytical Results

| Lab ID: Q197442100 | Date F | Received | : 10/30/ | 2019 1 | 2:15 | Ма | atrix: Drinking Wa | ter | | |
|----------------------------|-------------------------------|-----------|-----------|----------|----------|-----------------|--------------------|----------------|-----|----------|
| Sample ID: Gragg 3 | | Date C | Collected | : 10/28/ | 2019 1 | 1:55 Sa | mple T | ype: SAMPLE | | |
| Project ID: NEW WELL | BSEACD | | | | | | | | | |
| FIDJECTID. NEW WELL | BSEACD | | | | | | | | | |
| | | | | | | | | | | |
| Parameter | Results Units | MRL | LOD | | DF | Prepared | Ву | Analyzed | Ву | Qual |
| ALKALINITY (SM2320B, | Alkalinity) | | | | | | | | | |
| Phenolphthalein Alkalinity | 0.00 mg/L | 0.00 | 0.00 | | 1 | | | 11/01/19 00:00 | ME | * |
| Hydroxide Alkalinity | 0.00 mg/L | 0.00 | 0.00 | | 1 | | | 11/01/19 00:00 | ME | * |
| Bicarbonate Alkalinity | 249 mg/L | 0.00 | 0.00 | | 1 | | | 11/01/19 00:00 | ME | * |
| Carbonate Alkalinity | 0.00 mg/L | 0.00 | 0.00 | | 1 | | | 11/01/19 00:00 | ME | * |
| Total Alkalinity (CaCO3) | 249 mg/L | 20.0 | 20.0 | | 1 | | | 11/01/19 00:00 | ME | * |
| INORGANICS (E200.7 Pr | ep/E200.7 Metals, Trace Eleme | ents) | | | | | | | | |
| | | | | | | | | | | |
| Calcium Total | 65.0 mg/L | 0.200 | 0.0700 | | 1 | 11/04/19 14:48 | ME | 11/05/19 15:12 | FM | * |
| Iron Iotal | 0.217 mg/L | 0.0500 | 0.0200 | | 1 | 11/04/19 14:48 | ME | 11/05/19 15:12 | FM | |
| Sodium Total | 76.0 mg/L | 0.200 | 0.0700 | | 1 | 11/04/19 14:48 | ME | 11/05/19 15:12 | FM | |
| INORGANICS (E200.8, IC | P-MS Prep/E200.8, ICP-MS) | | | | | | | | | |
| Aluminum Total | <0.00500 mg/L | 0.00500 | 0.0020 | | 1 | 11/04/19 14:44 | ME | 11/07/19 11:13 | FO | |
| Arsenic Total | <0.00100 mg/L | 0.00100 | 0.0004 | 0.01 | 1 | 11/04/19 14:44 | ME | 11/07/19 11.13 | FO | |
| Copper Total | 0.00169 mg/L | 0.00100 | 0.0004 | 1 | 1 | 11/04/19 14:44 | ME | 11/07/19 11:13 | FO | |
| Lead Total | <0.00100 mg/l | 0.00100 | 0.0004 | 0.015 | 1 | 11/04/19 14:44 | ME | 11/07/19 11:13 | FO | |
| Manganese Total | 0.00519 mg/l | 0.00100 | 0.0004 | 0.015 | 1 | 11/04/19 14:44 | ME | 11/07/10 11:13 | FO | |
| Zinc Total | 0.399 mg/L | 0.00500 | 0.0020 | | 1 | 11/04/19 14:44 | ME | 11/07/19 11:13 | FO | |
| INORGANICS (E22/08 | lardnoss Calc) | | | | | | | | | |
| | | | | | | | | | | _ |
| Hardness, Calcium | 162 mg/L | | | | 1 | | | 11/06/19 09:09 | CW | |
| INORGANICS (E300.0, A | nions) | | | | | | | | | |
| Chloride | 45.9 mg/L | 1.00 | 0.500 | | 1 | | | 10/31/19 06:43 | ML | * |
| Fluoride | 1.80 mg/L | 0.0100 | 0.0050 | 4 | 1 | | | 10/31/19 06:43 | ML | * |
| Nitrite (as N) | <0.0100 mg/L | 0.0100 | 0.0050 | 1 | 1 | | | 10/31/19 06:43 | ML | * |
| Nitrate (as N) | <0.0100 mg/L | 0.0100 | 0.0050 | 10 | 1 | | | 10/31/19 06:43 | ML | * |
| Sulfate | 169 mg/L | 5.00 | 2.50 | | 5 | | | 10/31/19 16:27 | FO | |
| TOTAL DISSOLVED SOLIE | 9S (SM2540C, TDS) | | | | | | | | | |
| Total Dissolved | E69 | 25.0 | 10.0 | | 10 | | | 11/04/10 12:57 | 505 | <u> </u> |
| Solids(TDS) | 200 mg/L | 25.0 | 10.0 | | 10 | | | 11/04/19 13.57 | ERF | ¢ |
| рН (SM4500-H+B, pH @ | 25ºC) | | | | | | | | | |
| nH | 7 99 pH | 0.00 | 0.00 | | 1 | | | 11/07/19 08:32 | MF | * |
| Temperature | 21.0 c | 0.00 | 0.00 | | 1 | | | 11/07/19 08:32 | ME | * |
| P | | | | | | | | | | |
| Sample Comments | | | | | | | | | | |
| Sample Type: S/ | AMPLE | | | | | | | | | |
| • Gen | eral Comments for METHOD SM | Л4500-H+E | . pH - De | efined a | s a fiel | d parameter, me | asuren | nent must be | | |

taken within 15 minutes of collection. Results are provided for information purposes only.

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APPENDIX F: Water quality lab results & Isotope Geochemistry Results (Well #1)

Email information for report date: 2/28/18 17:11 B003298

Bee Cave Drilling

Attn: Bee Cave Drilling

185 Angel Fire Drive Dripping Springs, TX 78620

Happy New Year!

We at ATL appreciate your business and thank you for allowing us to partner in servicing your environmental needs.

Call or email us today at samplingbryan@aqua-techlabs.com for more information or to set up an event.

Sincerely, June M. Brien Executive Technical Director CORPORATE OFFICE 835 Phil Gramm Boulevard Bryan, TX 77807 Phone: (979) 778-3707 Fax: (979) 778-3183



AUSTIN OFFICE 7500 Hwy 71 W, Suite 105 Austin, TX 78735 Phone: (512) 301-9559 Fax: (512) 301-9552

SAP ACCA

TCEQ DW Lab ID TX 239

The analyses summarized in this report were performed by Aqua-Tech Laboratories, inc. unless otherwise noted. Aqua-Tech Laboratories, inc. holds accreditation from the State of Texas in accordance with TNI and/or through the TCEQ Drinking Water Commercial Laboratory Approval Program.

The following abbreviations indicate certification status:

- NEL TNI accredited parameter.
- ANR Accreditation not required by the State of Texas.
- DWP Accreditation through the TCEQ Drinking Water Commercial Laboratory Approval Program.
- INF Aqua-Tech Laboratories, inc. is not accredited for this parameter. It is reported on an informational basis only.

Subcontracted data summarized in this report is indicated by "Sub" in the Lab column.

General Definitions:

- NR Not Reported.
- RPD Relative Percent Difference.
- % R Percent Recovery.
- dry Results with the "dry" unit designation are reported on a "dry weight" basis.
- SQL The Sample Quantitation Limit is the value below which the parameter cannot reliably be detected. The SQL includes all sample preparations, dilutions and / or concentrations.
- Adj MDL The Adjusted Method Detection Limit is the MDL value adjusted for any sample dilutions or concentrations .
 - MDL The Method Detection Limit is the lowest theoretical value that is statistically different from zero for a specific method, taking into account all preparation steps and instrument settings.
- All samples are reported on an "as received" basis unless the designation "dry" is added to the reported unit.

Copies of Aqua-Tech Laboratories, Inc. procedures and individual sampling plans are available upon request. Note that samples are collected by Aqua-Tech Laboratories, Inc. personnel unless otherwise noted in the "Sample Collected" field of this reports s^Culture or "CLT".

Samples included in this report were received in acceptable condition according to Aqua-Tech Laboratories, inc. procedures and 40 CFR, Chapter I, Subchapter D, Part 136.3, TABLE II. - Required containers, preservation techniques, and holding times, unless otherwise noted in this report.

Record Retention

All reports, raw data, and associated quality control data are kept on file for 10 years before being destroyed. Any client that would like copies of records must contact Aqua-Tech Laboratories, inc. no later than six months prior to the scheduled disposal. An administrative fee for retrieval and distribution will apply.

This report was approved by:

Jene M. Brien June M. Brien, Technical Director

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CORPORATE OFFICE 685 Phil Gramm Boulevard



Analytical Report

| 035 Phil () | ramm Boulevard | | JA- | TECH | 7500 H | Wy 71 W, S | uite 105 | | | | Bee C | ave Drilling |
|-------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------|-------------------------|---------------------------------------------------------|-------------------|-----------------------------|--------------|-------------|------------------------|-------------------|-------------------|--------------|
| Elyan, 1X Phone: (9) | 7/80/ 791 778-3707 | | ROPATO | DRIES INC | Ph | Austin, 17 one: (512) 30 | C /8/85 | | | Report Printed: | 2/28/1 | 8 17:11 |
| Fax: (979) | 778-3193 | | JONAIN | Zittes, mo. | 1 | Fax: (512) 30 | 01-9552 | | | | | B003298 |
| | | | | | | | _ | • | | | | 2000200 |
| Gragg T | ract Pump Test 1 | | Collected: Received: | 02/01/18 12:30 by CLIENT 02/01/18 13:11 by Suzanne i | Rudd | | Type Grab | | Aratto | ng Water 2 | >-O-C # 184494 | |
| Lab ID# | B003298-01 | Result | Units | Notes | MDL | Adj MDL | 801. | Lab | Analyzed | Method | Batch | |
| General Ch | emistry | | | | | | | | | | | |
| Total Disc | olved Solids | 642 | mg/L | | 25.0 | 50.00 | 50.0 | Bryan | 02/07/18 16:32 BLR | 8M2540 C 2011 | M084200 | NEL. |
| Nitrate ac | N (NC3N) | 40,0500 | mg/L | | | 0.02 | 0.0500 | Austin | 02/06/18 13:10 MSA | 8M4500-NO3-F 2011 | [CALC] | MR. |
| Nitrite as | N | -9.01 | mg/L | J (0.001) | 0.001 | 0.00 | 0.01 | Austin | 02/02/18 07:55 M8A | 8M4500 NC2- B 200 | 0 M084064 | MR. |
| Nitrate/Ni | tite as N | 40.05 | mg/L | | 0.02 | 0.02 | 0.05 | Bryan | 02/06/18 13:10 MRB | 8M4500-NO3-F 2011 | M084124 | NF |
| Total Alka | linity as CaCOS (pH4.5) | 254 | mg/L | | 4.00 | 16.00 | 16.0 | Bryan | 02/06/18 14:34 MCP | 8M2320 B 2011 | M084154 | DHP |
| Fluoride | | 1.85 | mg/L | | 0.02 | 0.02 | 0.10 | Bryan | 02/09/18 12:18 MCP | 8M4500-F C 2011 | M084282 | |
| pH, Lab | | 7.3 | 8.0. | Hold-03 | | | NA | Austin | 02/05/18 12:04 KT | 8M4500-H+ B 2000 | M084102 | DHP |
| Temperat | ure @ pH Analysis | 18.6 | Deg. C | | | | NA | Austin | 02/05/18 12:04 KT | 8M2550 B 2000 | M084102 | MR |
| Metals (Tot | tal) | | | | | | | | | | | |
| Aluminun | 1 | 8.85 | ug/L. | | 0.299 | 0.31 | 1.03 | Bryan | 02/09/18 15:52 PNS | EPA 200.8 R5.4 | M084118 | NEL |
| Arcenio | | 0.714 | ug/L. | | 0.032 | 0.03 | 0.515 | Bryan | 02/09/18 15:52 PN8 | EPA 200.8 R5.4 | M084118 | MR. |
| Calolum | | 78.3 | mg/L | | 0.023 | 0.23 | 1.02 | Bryan | 02/14/18 17:12 PNS | EPA 200.7 R4.4 | M084229 | DHP |
| Copper | | 1.87 | ug/L. | | 0.029 | 0.03 | 0.515 | Bryan | 02/09/18 15:52 PNS | EPA 200.8 R5.4 | M084118 | <u>18</u> |
| Iron | | 0.431 | mg/L | | 0.002 | 0.00 | 0.102 | Bryan | 02/13/18 17:19 PNS | EPA 200.7 R4.4 | M084121 | MR. |
| Lead | | 0.785 | ug/L. | | 0.005 | 0.01 | 0.515 | Bryan | 02/09/18 15:52 PN8 | EPA 200.8 R5.4 | M084118 | NR. |
| Manganee | 10 | 4.38 | ug/L. | | 0.108 | 0.11 | 0.515 | Bryan | 02/09/18 15:52 PN8 | EPA 200.8 R5.4 | M084118 | <u>MR.</u> |
| Sodium | | 32.6 | mg/L | | 0.011 | 0.11 | 1.02 | Bryan | 02/08/18 21:19 PNS | EPA 200.7 R4.4 | M084229 | NR. |
| Zino | | 327 | ug/L. | M8-01 | 0.379 | 0.39 | 4.12 | Bryan | 02/09/18 15:52 PN8 | EPA 200.8 R5.4 | M084118 | NR. |
| Drinking W | ater Metals (Total) | | | | | | | | | | | |
| Calolum H | lardness as CaCO3 | 196 | mg/L | | | 0.59 | 2.55 | Bryan | 02/14/18 17:12 PNS | EPA 200.7 R4.4 | [CALC] | ANR |
| General Ch | emistry | | | | | | | | | | | |
| Suffate ac | 804 | 162 | mg/L | | 0.01 | | 3 | Sub | 02/02/18 14:41 ANA | EPA 300.0 | SUB | NEL. |
| Chioride | | 19 | mg/L | | 0.02 | | 3 | Sub | 0202/18 14:41 ANA | EPA 300.0 | SUB | MR. |
| | | | | Đ | planatio | on of Note | 25 | | | | | |
| A-01 | Optional LCSD was | outside expected range, o | ausing RPD to i | be greater than expected. By | • esuits acced | ited on one r | equired or | essing LCS | and sample matrix RPD. | | | |
| A-01a | Optional LC3D was | outside expected range | Results accente | d on one required passion I (| 18 | | | | | | | |
| Hold-03 | This parameter was | outside of EPA holding at | the time the sar | mple was received in the labo | ratory. | | | | | | | |
| J | Analyte detected bei | ow the SQL but above the | MDL | | | | | | | | | |
| M9-01 | The college of the co | an autoida accestrante lite | alls for the 147 - | andles MOD. The balch was | accepted by | | ninini i C | O and loc 1 | | | | |
| | The spike recovery w | vas outside acceptance li | nits for the MS (| anulor MSD. The batch Was | accepted ba | ised on acce | pable LG | o anavor Li | Lou recovery. | | | |

Form: C. ELMNTVFORMATVATL 122117 FIN_L&RPT

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| Laboratory Services | 1 | | | LCRA Enviro | nmental Laboratory Ser 3505 Montopolis Austin, TX 7 Phone: (512) 730- Fax: (512) 730- |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------|-------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------|
| BETA B | Beta Analytic Inc 4985 SW 74 Court Miami, Florida 33155 Tel: 305-667-5167 Fax: 305-663-0964 info@betalabservices.com | | | | |
| | ISO/IEC 17025:2 | 005-Accredited Testing L | aboratory | | |
| Dale Jurecka | | | | Rep | ort Date: 9/23/2019 |
| CRA-Environmental Laboratory | Services (EL-101) | | | Material | Received: 9/9/2019 |
| Sample Data | рМС | F ¹⁴ C | d13C o/oo | d180 o/oo | dD o/oo |
| leta - 536533 | < 0.44 pMC | < 0.0044 | -0.50 | -4.64 | -24.46 |
| 21960710001 MS-Standard delivery IATERIAL/PRETREATMENT: (w COMMENTS: The equivalent "App ny hydro-geochemical effects on reasurements within 1-2 pMC are (CO3) DIC14 and waters with co | vater DIC) acidify-gas strip parent" radiocarbon age to 1 meteoric water 14CO2). G e reasonable for a single wa molex organic chemistry, re | the reported pMC/IMDN valu siven the complex nature of g after sample. For very low DIG suits can very significantly o | es is ~ > 43500 B groundwater DIC 1- C concentration wa utside of this expe | P BP (not adjuste 4 chemistry, dupl aters (< 20 mg/L ectation. | ad for icate |
| leta - 536534 | 0.60 +/- 0.04 pMC | D,0060 +/- D.0004 | -4.80 | -4.58 | -24.36 |
| 1990/71002 MS-Standard delivery IATERIAL/PRETREATMENT: (w IOMMENTS: The equivalent "Ap ydro-geochemical effects on met reasurements within 1-2 pMC arr | rater DIC) acidify-gas strip parent" radiocarbon age to l seorio water 14CO2). Cliven e reasonable for a single wa | the reported pMC/fMDN valu the complex nature of group ater sample. For very low DIG | ies is ~ 41100 BP ndwater DIC14 ch 2 concentration wa | (not adjusted for emistry, duplicate aters (< 20 mg/L | 90-755 any |

| Client: LCRA ENVIRONMENTAL | LAB SERVICES | Pu | rchase Order: Q19 | 60711 |
|----------------------------|----------------|---------------|-------------------|----------------|
| Recvd : 19/09/05 | | Contact: Dale | Jurecka, 512/356 | -6022 |
| Job# : 3839 | | 3505 1 | Montopolis Dr (f) | -6021 |
| Final : 19/11/20 | envlab@lcra.o: | rg | Austin, TX | 78744 |
| | | | | |
| Cust LABEL INFO | JOB.SX R | EFDATE QUANT | ELYS TU | eTU |
| | | | | |
| Q1960711001 | 3839.01 | 190828 1000 | 275 0.03 | 0.0968-08-206 |
| Q1960711002 | 3839.02 | 190828 1000 | 275 -0.05 | 0.0958-50-755 |
| Q1960711003 | 3839.03 | 190828 1000 | 275 -0.05 | 0.0968-08-205 |
| Q1960711004 | 3839.04 | 190829 1000 | 275 1.46 | 0.09 57-40-304 |
| | | | | |

| | ABOR/TORIES INC | ANALY | SIS R | EPORT | 19 ¹⁰ |
|-------------------------------------------------|----------------------------------------------|--------------------|-----------|------------------------|------------------|
| Lab #: Sample Name: Company: API/Well: | 732787 Job Q1960713002 LCRA Environmer | #: 42696 I | IS-64056 | Co. Job#: Co. Lab#: | |
| Container: Field/Site Name: Location: | Plastic Bottle 45324066 | | | 58-50-755 | |
| Sampling Point: Date Sampled: | 8/28/2019 14:10 | Date Received: | 9/04/2019 | Date Reported: | 9/13/2019 |
| δD of water | | -24.6 ‰ relative t | D VSMOW | | |
| δ ¹⁸ O of water | | -4.44 ‰ relative t | D VSMOW | | |
| Tritium content of | water | na | | | |
| δ ¹³ C of DIC | | na | | | |
| ¹⁴ C content of DIC | | na | | | |
| δ ¹⁵ N of nitrate | | na | | | |
| $\delta^{18}O$ of nitrate | | na | | | |
| δ ³⁴ S of sulfate | | na | | | |
| $\delta^{18}O$ of sulfate | | na | | | |
| Vacuum Distilled? | • | No | | | |
| Remarks: | | | | | |

nd = not detected. na = not analyzed. *Indicates if vacuum distillation was utilized for hydrogen and oxygen isotopic analysis of water



Massachusetts Institute of Technology

Date: 10/14/2019

Analysts: Ryan Frazer and Jahan Ramezani

| Sample # | Sample Type | ⁸⁷ Sr/ ⁸⁶ Sr | % std err | 2σ std err |
|-------------|-------------|------------------------------------|-----------|--------------------|
| Sample # | Sample Type | (1) | (2 | 2) |
| Q1960712001 | water | 0.707606 | 0.00074 | 1.05E-05 68-08-206 |
| Q1960712002 | water | 0.708372 | 0.00088 | 1.25E-05 58-50-755 |
| Q1960712003 | water | 0.707904 | 0.00071 | 1.01E-05 68-08-205 |
| Q1960712004 | water | 0.709376 | 0.00092 | 1.30E-05 57-40-304 |
| | | | | |

(1) Corrected for mass-dependant fractionation.

(2) Within-run internal precision of measured ratio.

Long term reproducibility of NBS-987 Sr standard at MIT: 0.7102379 ± 0.0000109 (2 σ s.e.).